

Basics of 3D EM IE modelling

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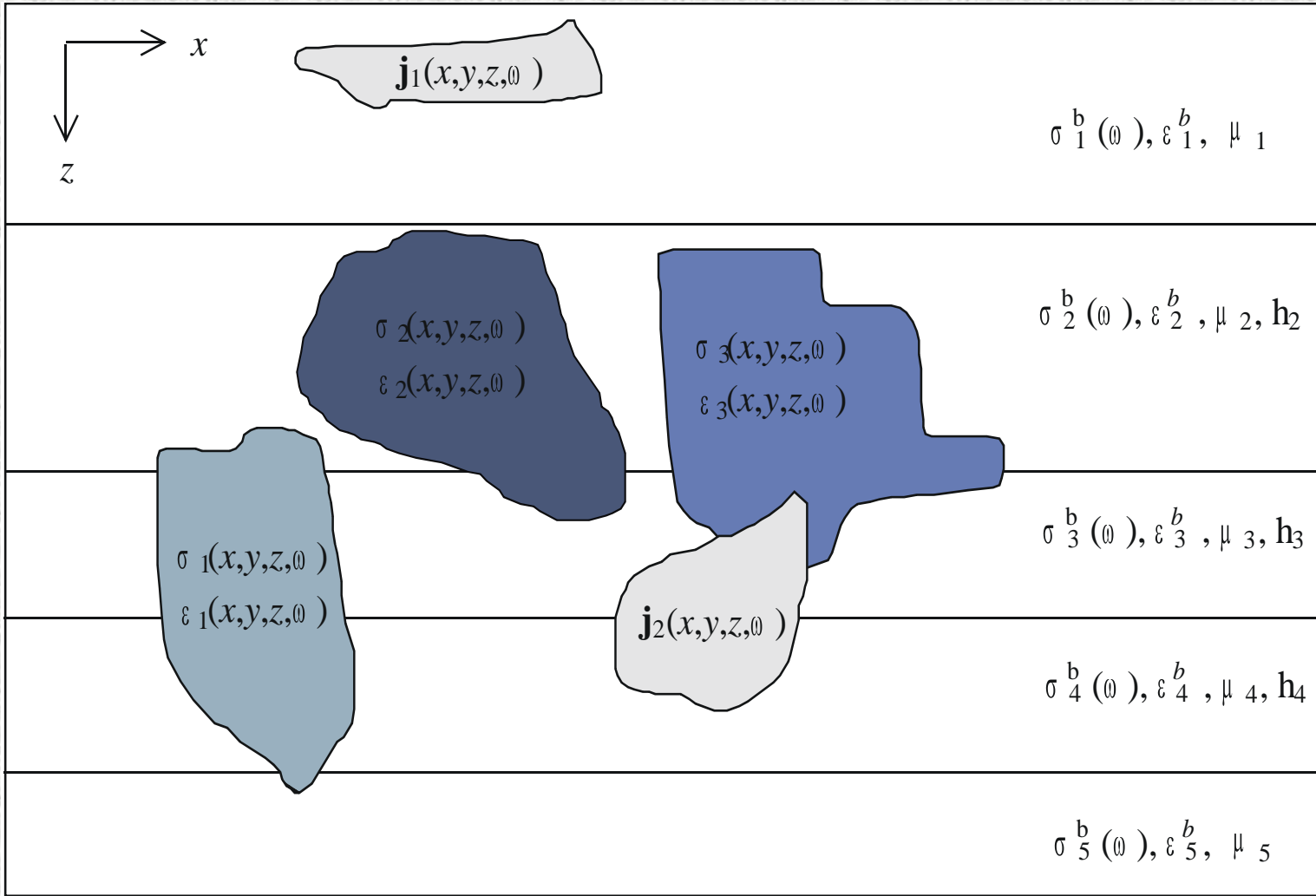


Fig. Example of a 3D problem (side view).

Maxwell's equations in frequency-domain

$$\underline{\nabla} \times \underline{\mathbf{H}} = \underline{\zeta}(\underline{\mathbf{x}}, \underline{\mathbf{y}}, \underline{\mathbf{z}}, \omega) \underline{\mathbf{E}} + \underline{\mathbf{j}}^{\text{ext}}, \quad \underline{\nabla} \times \underline{\mathbf{E}} = i\omega \underline{\mu}(\underline{\mathbf{z}}) \underline{\mathbf{H}}$$

$$\underline{\zeta}(\underline{\mathbf{x}}, \underline{\mathbf{y}}, \underline{\mathbf{z}}, \omega) = \underline{\underline{\sigma}} - i\omega \underline{\underline{\epsilon}} = \begin{pmatrix} \zeta_{xx} & 0 & 0 \\ 0 & \zeta_{yy} & 0 \\ 0 & 0 & \zeta_{zz} \end{pmatrix} \quad \underline{\underline{\mu}}(\underline{\mathbf{z}}, \omega) = \begin{pmatrix} \mu_x & 0 & 0 \\ 0 & \mu_y & 0 \\ 0 & 0 & \mu_z \end{pmatrix}$$

Maxwell's equations for reference EM field

$$\underline{\nabla} \times \underline{\mathbf{H}}^0 = \underline{\zeta}_0(\underline{\mathbf{z}}, \omega) \underline{\mathbf{E}}^0 + \underline{\mathbf{j}}^{\text{ext}}, \quad \underline{\nabla} \times \underline{\mathbf{E}}^0 = i\omega \underline{\mu}(\underline{\mathbf{z}}) \underline{\mathbf{H}}^0.$$

$$\underline{\zeta}_0(\underline{\mathbf{z}}, \omega) = \begin{pmatrix} \zeta_{0xx} & 0 & 0 \\ 0 & \zeta_{0yy} & 0 \\ 0 & 0 & \zeta_{0zz} \end{pmatrix}$$

Maxwell's equations for scattered EM field

$$\underline{\nabla} \times \underline{\mathbf{H}}^s = \underline{\zeta}_0(\underline{\mathbf{z}}, \omega) \underline{\mathbf{E}}^s + \underline{\mathbf{j}}^s, \quad \underline{\nabla} \times \underline{\mathbf{E}}^s = i\omega \underline{\mu}(\underline{\mathbf{z}}) \underline{\mathbf{H}}^s.$$

$$\underline{\mathbf{j}}^s = (\underline{\zeta} - \underline{\zeta}_0) (\underline{\mathbf{E}}^s + \underline{\mathbf{E}}^0).$$

$$\underline{\nabla} \times \frac{1}{i\omega} \underline{\mu}^{-1}(\underline{\mathbf{z}}) \underline{\nabla} \times \underline{\mathbf{E}}^s - \underline{\zeta}_0(\underline{\mathbf{z}}, \omega) \underline{\mathbf{E}}^s = \underline{\mathbf{j}}^s \iff \underline{\mathbf{E}}^s(\underline{\mathbf{r}}) = \int_{V^s} \underline{\underline{G}}_0^s(\underline{\mathbf{r}}, \underline{\mathbf{r}}') \underline{\mathbf{j}}^s(\underline{\mathbf{r}}') d\underline{\mathbf{v}}'$$

$$\underline{\mathbf{r}} = (x, y, z), \quad d\underline{\mathbf{v}}' = dx' dy' dz'$$

Conventional scattering equation (Dmitriev, 1969; Weidelt, 1975)

$$\underline{\mathbf{E}}^s(\underline{\mathbf{r}}) = \underline{\mathbf{E}}_0 + \underline{Q} \underline{\mathbf{E}}^s = \underline{\mathbf{E}}_0(\underline{\mathbf{r}}) + \int_{V^s} \underline{\underline{G}}_0^s(\underline{\mathbf{r}}, \underline{\mathbf{r}}') (\underline{\zeta}(\underline{\mathbf{r}}') - \underline{\zeta}_0(\underline{\mathbf{z}}')) \underline{\mathbf{E}}^s(\underline{\mathbf{r}}') d\underline{\mathbf{v}}' \quad (1)$$

3x3 dyadic for the electric-to-electric Green's function of the 1D reference formation:

$$\underline{\underline{G}}_0^s = \begin{pmatrix} G_{xx} & G_{xy} & G_{xz} \\ G_{yx} & G_{yy} & G_{yz} \\ G_{zx} & G_{zy} & G_{zz} \end{pmatrix}$$

Formal solution of eq. (1) can be expressed as an infinite Neumann series

$$\underline{\mathbf{E}}^s(\underline{\mathbf{r}}) = (1 - \underline{Q})^{-1} \underline{\mathbf{E}}_0 = \underline{\mathbf{E}}_0 + \underline{Q} \underline{\mathbf{E}}_0 + \underline{Q}^2 \underline{\mathbf{E}}_0 + \dots$$

As a rule, the series doesn't converge at all.

Conventional scattering equation

$$\mathbf{E}^s(\mathbf{r}) = \mathbf{E}_o + Q\mathbf{E}^s = \mathbf{E}_o(\mathbf{r}) + \int_{V^s} \underline{\underline{G}}_o^s(\mathbf{r}, \mathbf{r}') (\underline{\underline{\zeta}}(\mathbf{r}') - \underline{\underline{\zeta}}_o(z')) \mathbf{E}^s(\mathbf{r}') dV'$$

$$\mathbf{E}^s \rightarrow \chi:$$

$$\chi = \frac{1}{2} \lambda^{-1} ((\underline{\underline{\zeta}} + \underline{\underline{\zeta}}^*) \mathbf{E}^s + (\underline{\underline{\zeta}} - \underline{\underline{\zeta}}_o) \mathbf{E}_o)$$

$$\underline{\underline{\lambda}}(\mathbf{z}, \mathbf{z}) = \begin{pmatrix} \sqrt{\text{Re}\zeta_{o\tau}} & 0 & 0 \\ 0 & \sqrt{\text{Re}\zeta_{o\tau}} & 0 \\ 0 & 0 & \sqrt{\text{Re}\zeta_{oz}} \end{pmatrix}$$

Scattering equation MIDM (Singer, 1995; Pankratov, Avdeev, Kuvshinov, 1995; Pankratov, Kuvshinov, Avdeev, 1997; Singer & Fainberg, 1995, 1997)

$$\chi(\mathbf{r}) = \chi_o + M\chi = \chi_o(\mathbf{r}) + \int_{V^s} \underline{\underline{K}}(\mathbf{r}, \mathbf{r}') \underline{\underline{R}}(\mathbf{r}') \chi(\mathbf{r}') dV'$$

$$\underline{\underline{K}}(\mathbf{r}, \mathbf{r}') = \delta(\mathbf{r} - \mathbf{r}') \mathbb{1} + 2\underline{\underline{\lambda}}(\mathbf{z}) \underline{\underline{G}}_o^s(\mathbf{r}, \mathbf{r}') \underline{\underline{\lambda}}(z')$$

$$\underline{\underline{R}}(\mathbf{r}) = (\underline{\underline{\zeta}}(\mathbf{r}) - \underline{\underline{\zeta}}_o(z)) (\underline{\underline{\zeta}}(\mathbf{r}) + \underline{\underline{\zeta}}_o^*(z))^{-1}$$

$$\chi = (1 - M)^{-1} \chi_o = \chi_o + M\chi_o + M^2\chi_o + \dots$$

The Neumann's series converges for any frequency and any electrical resistivity contract $\|\underline{\underline{M}}\chi\| < \|\chi\| \quad \forall \chi$

Simple iteration (MIDM; Avdeev et al., 2000)

$$\chi^{(n+1)} = \chi_o + M\chi^{(n)}, \quad n=1, 2, \dots$$

Krylov iteration (Avdeev et al., 2002)

$$A\chi = \chi_o,$$

$$A = 1 - M.$$

$$\kappa(A) = \|A\| \|A^{-1}\| \leq \sqrt{C_1} \quad (C_1 = 10^4 \Rightarrow \kappa(A) \leq 10^2)$$

EM field determination

$\chi \rightarrow \mathbf{j}^q$

$$\mathbf{j}^q(\mathbf{r}) = 2\underline{\underline{\lambda}}(\underline{\underline{\zeta}} + \underline{\underline{\zeta}}^*)^{-1}(\underline{\underline{\zeta}} - \underline{\underline{\zeta}}_0)(\underline{\underline{\chi}} + \underline{\underline{\lambda}}\mathbf{E}^0), \quad \mathbf{r} \in V^S$$

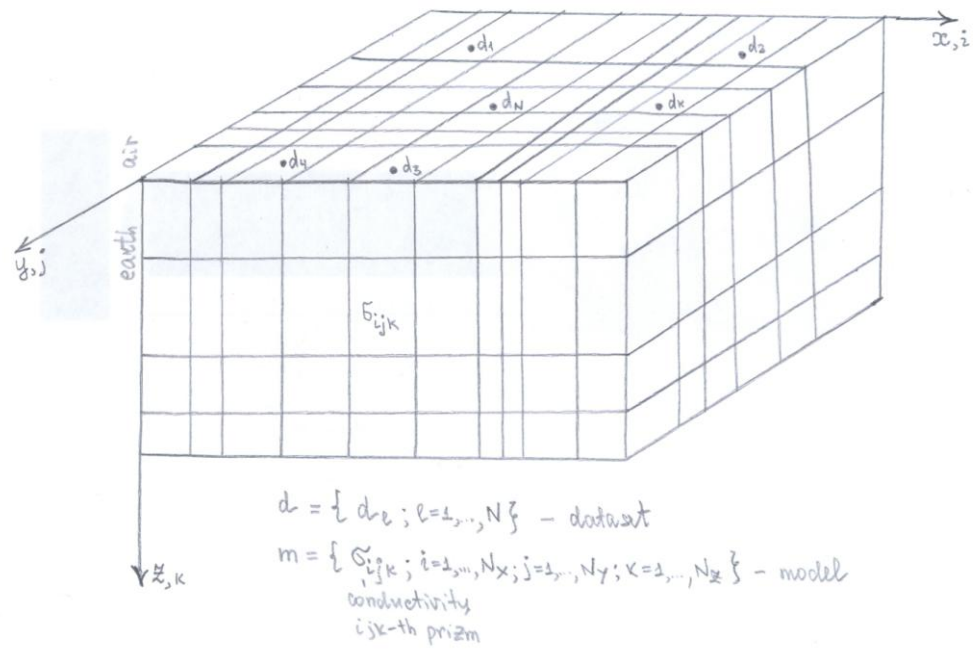
$\mathbf{j}^q \rightarrow \mathbf{E}^S, \mathbf{H}^S$

$$\nabla \times \frac{1}{i\omega} \underline{\underline{\mu}}^{-1}(z) \nabla \times \mathbf{E}^S - \underline{\underline{\zeta}}_0(z, \omega) \mathbf{E}^S = \mathbf{j}^q.$$

$$\mathbf{E}^S(\mathbf{r}) = \int_{V^S} \underline{\underline{G}}_0^{ee}(\mathbf{r}, \mathbf{r}') \mathbf{j}^q(\mathbf{r}') dv', \quad \mathbf{H}^S(\mathbf{r}) = \int_{V^S} \underline{\underline{G}}_0^{me}(\mathbf{r}, \mathbf{r}') \mathbf{j}^q(\mathbf{r}') dv',$$

$$\mathbf{E} = \mathbf{E}^0 + \mathbf{E}^S, \quad \mathbf{H} = \mathbf{H}^0 + \mathbf{H}^S(\mathbf{r}).$$

Fig. A 3-D MT model discretized with rectangular prisms.



(1) Integral equation (IE) approach

$$\chi(\mathbf{r}) = \chi^d(\mathbf{r}) + \int_{V^s} \underline{\underline{K}}(\mathbf{r}, \mathbf{r}') \underline{\underline{R}}(\mathbf{r}') \chi(\mathbf{r}') d\mathbf{v}'$$

$A_{IE} \cdot \mathbf{x} = \mathbf{b}$ - system of linear equations (\leftarrow on a rectangular 3-D grid);

A_{IE} - complex, dense with all entries filled, non-Hermitian matrix; but much more compact than FD and FE matrices

(a) Main attraction: only the scattering volume V^s is subject to discretization;

(this reduce dramatically the size of matrix A_{IE})

(b) Drawback: most EM software developers refrain from implementation of the IE approach, since

accurate computation of the matrix A_{IE} is indeed an extremely tedious and nontrivial problem itself.

$$\nabla \times \underline{\mu}^{-1} \underline{E} - i\omega \underline{\zeta}(x, y, z, \omega) \underline{E} = \underline{j}^{ext}$$

(2) Finite-difference (FD) approach

$\underline{A}_{FD} \cdot \underline{x} = \underline{b}$ - system of linear equations (← on a rectangular 3D grid);

\underline{A}_{FD} - large, sparse 3Mx3M symmetric, non-Hermitian matrix;

\underline{x} represents the grid nodal values of electric field;

\underline{b} represents the source and boundary conditions

$M = n_x \cdot n_y \cdot n_z$ - number of model parameters.

- (a) The most commonly employed
- (b) Main attraction: an apparent simplicity of its numerical implementation

(3) Finite-element (FE) approach

the EM field (or its potentials) are decomposed to some basic (usually, edge and nodal) functions. The coefficients of the decomposition, a vector \underline{x} , are sought using the Galerkin method

$$\underline{A}_{FE} \cdot \underline{x} = \underline{b}$$

\underline{A}_{FE} - large, sparse, non-symmetric, non-Hermitian matrix;

- (a) Main attraction: it is commonly believed to be better able than other approaches to accurately account for geometry (shapes of ore-bodies, topography, cylindrical wells, etc.)
- (b) Main drawback: construction of the finite elements themselves is another nontrivial and usually time-consuming procedure.

Based on the above approach, there have been developed 3D forward modeling solutions for various EM applications

- ✓ Induction logging in deviated boreholes
- ✓ Airborne electromagnetics
- ✓ General controlled-source EMs, MT, and CSMT
- ✓ Global induction studies

The solutions:

- give accurate results even for lateral contrast of electrical resistivity up to 100,000;
- simulate the frequency-domain responses in frequency range from DC up to 50 MHz;
- account for the induced polarization and displacement currents;
- admit an *anisotropy* of the electrical conductivity;
- allow to run large-scale models discretized by up to 1,000,000 cells;

Thank you for your
attention