Introduction to x3d integral equation code

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•x3d theory •Comparison with other approaches •example

•x3d theory · Companison with other approaches • ezemple

Complex-valued conductivity

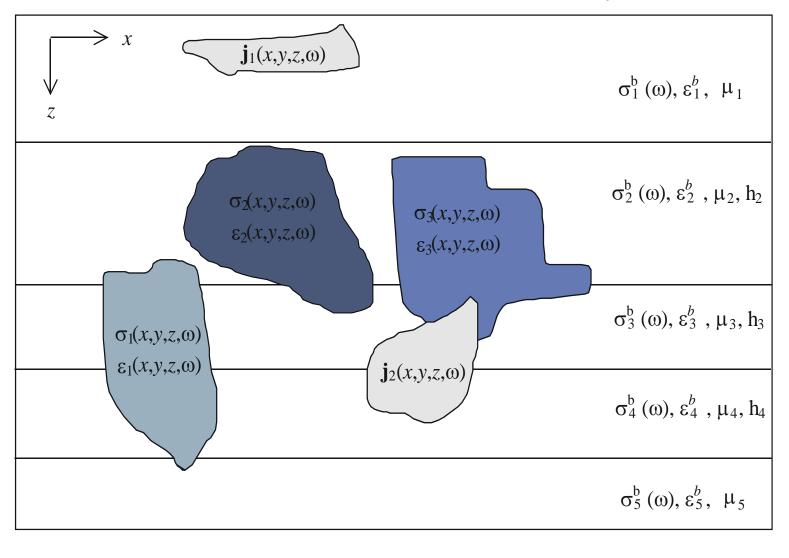


Fig. Example of a 3D model (side view) to be handled by x3d.

x3d code maths

$$\nabla \times \mathbf{H} = \underline{\zeta}(x, y, z, \omega) \mathbf{E} + \mathbf{j}^{ext}, \quad \nabla \times \mathbf{E} = i\omega\mu(z)\mathbf{H}$$

$$\underline{\zeta}(x, y, z, \omega) = \underline{\sigma} - i\omega\underline{\xi} = \begin{bmatrix} \zeta_{xx} & 0 & 0 \\ 0 & \zeta_{yy} & 0 \\ 0 & 0 & \zeta_{zz} \end{bmatrix}, \quad \mu(z, \omega) = \begin{bmatrix} \mu_{\tau} & 0 & 0 \\ 0 & \mu_{\tau} & 0 \\ 0 & 0 & \mu_{z} \end{bmatrix},$$
Maxwell's equations for reference EM field
$$\nabla \times \mathbf{H}^{o} = \underline{\zeta}(z, \omega)\mathbf{E}^{0} + \mathbf{j}^{ext}, \quad \nabla \times \mathbf{E}^{0} = i\omega\mu(z)\mathbf{H}^{0}, \quad \underline{\zeta}_{0}(z, \omega) = \begin{bmatrix} \zeta_{0\tau} & 0 & 0 \\ 0 & \zeta_{0\tau} & 0 \\ 0 & 0 & \zeta_{0z} \end{bmatrix},$$
Maxwell's equations for scattered EM field
$$\nabla \times \mathbf{H}^{s} = \underline{\zeta}(z, \omega)\mathbf{E}^{s} + \mathbf{j}^{q}, \quad \nabla \times \mathbf{E}^{s} = i\omega\mu(z)\mathbf{H}^{s}, \quad \mathbf{j}^{q} = (\underline{\zeta} - \underline{\zeta})(\mathbf{E}^{s} + \mathbf{E}^{s}).$$

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$$\nabla \times \mathbf{H}^{s} = \underline{\zeta}(z, \omega)\mathbf{E}^{s} = \mathbf{j}^{q} \quad \mathbf{E}^{s}(\mathbf{r}) = \int_{\mathbf{Z}} \underline{G}_{e^{s}}^{ee}(\mathbf{r}, \mathbf{r}^{s})\mathbf{j}^{q}(\mathbf{r}^{s})dv^{s}.$$

$$\mathbf{r}^{s}(\mathbf{r}) = \mathbf{E}_{o} + Q\mathbf{E}^{s} = \mathbf{E}_{o}(\mathbf{r}) + \underbrace{\int_{\overline{Z}} \underline{G}_{e^{s}}^{ee}(\mathbf{r}, \mathbf{r}^{s})(\underline{\zeta}(\mathbf{r}^{s}) - \underline{\zeta}_{0}(z))\mathbf{E}^{s}(\mathbf{r})dv^{s}.$$

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$$\mathbf{E}^{s}(\mathbf{r}) = \mathbf{E}_{o} + \mathbf{E}_{o} + \mathbf{E}_{o} + \mathbf{E}_{o} + \mathbf{E}_{o} + \mathbf{E}_{o}$$

3x3 dyadic for the electric-to-electric Green's function of the 1D reference formation:

Formal solution of eq. (1) can be expressed as an infinite Neumann series

$$\mathbf{E}^{\mathrm{s}}(\mathbf{r}) = (1 - Q)^{-1} \mathbf{E}_{o} = \mathbf{E}_{o} + Q \mathbf{E}_{o} + Q^{2} \mathbf{E}_{o+\dots}$$

As a rule, the series doesn't converge at all.

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x3d code maths

$$\mathbf{E}^{s} \rightarrow \chi$$
:

Scattering equation MIDM (Singer, 1995; Pankratov, Avdeev, Kuvshinov, 1995; Pankratov, Kuvshinov, Avdeev, 1997; Singer & Fainberg, 1995, 1997)

$$\chi(\mathbf{r}) = \chi_{o} + M\chi = \chi_{o}(\mathbf{r}) + \int \underline{K}(\mathbf{r},\mathbf{r}')\underline{R}(\mathbf{r}')\chi(\mathbf{r}')dv'$$

$$V^{S}$$

$$\underline{K}(\mathbf{r},\mathbf{r}') = \delta(\mathbf{r}-\mathbf{r}')\underline{1} + 2\underline{\lambda}(z)\underline{G}_{o}^{ee}(\mathbf{r},\mathbf{r}')\underline{\lambda}(z')$$

$$\underline{\underline{R}}(\mathbf{r}) = \left(\underline{\zeta}(\mathbf{r}) - \underline{\zeta}_{=0}(z)\right) \left(\underline{\zeta}(\mathbf{r}) + \underline{\zeta}_{=0}^{*}(z)\right)^{-1}$$

$$\chi = (1 - M)^{-1} \chi_o = \chi_o + M \chi_o + M^2 \chi_{o+...}$$

The Neumann's series converges for any frequency and any electrical resistivity contract

 $\left\|\underline{\underline{M}}_{\mathcal{X}}\right\| < \|\mathcal{X}\|, \quad \forall \mathcal{X}$

Simple iteration (MIDM; Avdeev et al., 2000)

$$\chi^{(n+1)} = \chi_0 + M \chi^{(n)}, n=1,2,...$$

Krylov iteration (Avdeev et al., 2002)

$$A\chi = \chi_{0}, \qquad A = 1 - M.$$

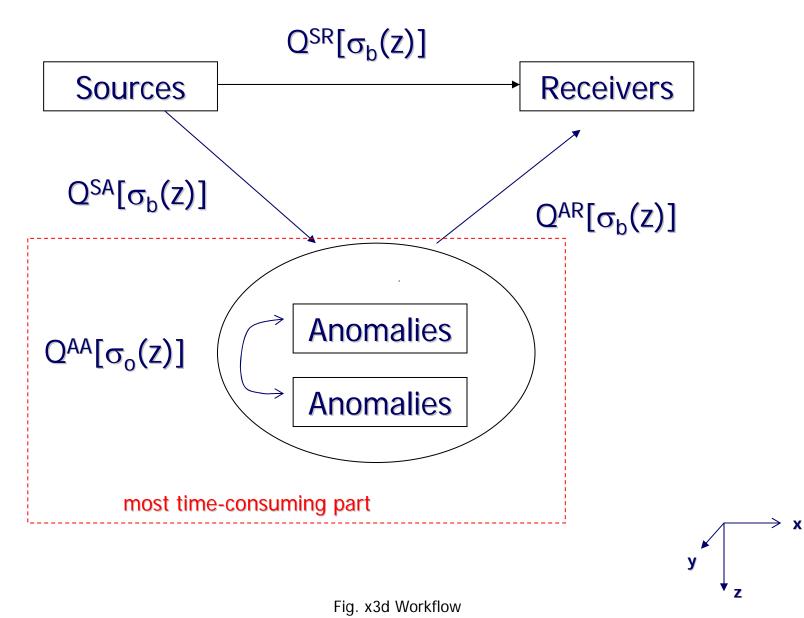
$$\kappa(A) = \|A\| \|A^{-1}\| \leq \sqrt{C_{l}} \qquad (C_{l} = 10^{4} \Rightarrow \kappa(A) \leq 10^{2})$$

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EM field calculation

$$\begin{split} \boldsymbol{\chi} \rightarrow \mathbf{j}^{q} & \mathbf{j}^{q}(\mathbf{r}) = 2 \underbrace{\lambda} (\underline{\zeta} + \underline{\zeta}^{*})^{-1} (\underline{\zeta} - \underline{\zeta}) (\boldsymbol{\chi} + \underbrace{\lambda} \mathbf{E}^{0}), \quad \mathbf{r} \in V^{S} \\ \mathbf{j}^{q} \rightarrow \mathbf{E}^{S}, \mathbf{H}^{S} & \nabla \times \frac{1}{i\omega} \underbrace{\mu}^{-1}(z) \nabla \times \mathbf{E}^{S} - \underbrace{\zeta}_{o}(z, \omega) \mathbf{E}^{S} = \mathbf{j}^{q}. \\ \mathbf{E}^{S}(\mathbf{r}) = \int \underbrace{G}_{o}^{ee}(\mathbf{r}, \mathbf{r}') \mathbf{j}^{q}(\mathbf{r}') dv', \quad \mathbf{H}^{S}(\mathbf{r}) = \int \underbrace{G}_{o}^{me}(\mathbf{r}, \mathbf{r}') \mathbf{j}^{q}(\mathbf{r}') dv', \\ \mathbf{V}^{S} & V^{S} \\ \mathbf{E} = \mathbf{E}^{0} + \mathbf{E}^{S}, \quad \mathbf{H} = \mathbf{H}^{0} + \mathbf{H}^{S}(\mathbf{r}). \end{split}$$





x3d code

x3d_64x64x32_RM.exe
x3d_125x125x16_RM.exe
x3d_125x125x64_HD.exe
x3d_256x256x8_RM.exe
x3d_256x256x32_HD.exe
x3d_350x350x16_HD.exe
x3d_350x350x16_HD.exe

Fig. x3d grids available on 32-bit Windows machines.

On 64-bit computers maximum grids are far larger.

Fig. x3d screen output example

Code requires 22 MegaBytes of disk spa	100	Slide 6
including 11 MegaBytes for Greens	matrices	
run # 1 of 2	polarization # 1 of	2
Nx x Ny x Nz : 40 x 40 x 5 model file : "01.model" frequency : 0.100000 [Hz]		
Computes Greens matrices (a2a) Computes Greens matrices Computes En (at A) Computes j^s=(zeta-zeta^N)*En on A Krylov subspaces iteration (GPBi-CGZW) Computes free term free term norm = 5.00E+05 iter residual 1 8.009E-01 2 4.290E-01 3 2.954E-01 4 2.216E-01 5 1.422E-01 6 1.176E-01 7 7.474E-02 8 6.251E-02 9 2.904E-02 10 2.126E-02 11 1.936E-02 12 1.595E-02 13 1.359E-02 14 1.080E-02 15 7.777E-03 16 6.097E-03 17 3.702E-03 18 2.995E-03 19 2.834E-03 20 2.159E-03 21 1.730E-03 22 1.389E-03 23 1.059E-03 24 9.237E-04 Computes Greens scalars Computes Greens matrices Convolutes (a2o) Computes Greens matrices Convolutes (a2o)	$\begin{array}{c} 15.17.24.\\ 15.17.24.\\ 15.17.27.\\ 15.17.31.\\ 15.17.31.\\ 15.17.31.\\ 15.17.31.\\ 15.17.32.\\ 15.17.34.\\ 15.17.35.\\ 15.17.36.\\ 15.17.36.\\ 15.17.37.\\ 15.17.38.\\ 15.17.38.\\ 15.17.41.\\ 15.17.42.\\ 15.17.43.\\ 15.17.43.\\ 15.17.44.\\ 15.17.45.\\ 15.17.45.\\ 15.17.46.\\ 15.17.47.\\ 15.17.50.\\ 15.17.51.\\ 15.17.51.\\ 15.17.51.\\ 15.17.55.\\ 15.17.57.\\ 15.17.57.\\ 15.17.57.\\ 15.17.57.\\ 15.17.57.\\ 15.17.58.\\ 15.17.59.\\ 15.17.59.\\ 15.17.59.\\ 15.17.59.\\ 15.17.59.\\ 15.17.59.\\ 15.18.4.\\ 15.18.5.\\ 15.18.5.\\ 15.18.5.\\ 15.18.8.\\ 15.18.5.\\ 15.18.8.$	27.10.200 27.10.201
run # 1 of 2 Nx x Ny x Nz : 40 x 40 x 5 model file : "01.model"	polarization # 2 of	2
frequency : 0.100000 [Hz] Computes En (at A) Computes j^s=(zeta-zeta^N)*En on A Krylov subspaces iteration (GPBi-CGZW) Computes free term free term norm = 5.14E+05	15.18.8. 15.18.8. 15.18.8. 15.18.8. 15.18.8. 15.18.9.	27.10.200 27.10.200 27.10.200 27.10.200 27.10.200 27.10.200

Based on the above IE approach, there have been developed 3D forward modeling solutions for various EM applications

- Induction logging in deviated boreholes
- ✓ Airborne electromagnetics
- ✓ General controlled-source EMs, MT, and CSMT
- ✓ Global induction studies

The solutions:

- give accurate results even for lateral contrast of electrical resistivity up to 100,000;
- simulate the frequency-domain responses in frequency range from DC up to 50 MHz;
- account for the induced polarization and displacement currents;
- admit an *anisotropy* of the electrical conductivity;
- allow to run large-scale models discretized to 1,000,000 cells at 32-bit machines;

•23d theony · Comparison with other approaches

•ezemple

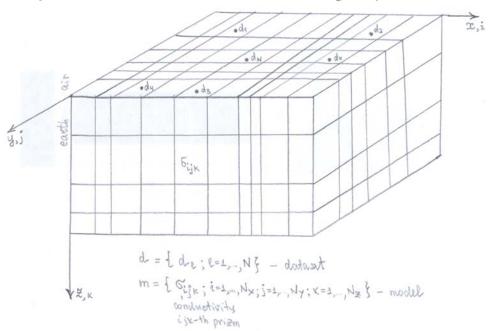
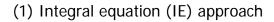


Fig. A 3-D MT model discretized with rectangular prisms.



$$\chi(\mathbf{r}) = \chi_0(\mathbf{r}) + \int \underline{K}(\mathbf{r},\mathbf{r}')\underline{R}(\mathbf{r}')\chi(\mathbf{r}')dv'$$

 $A_{\mu} \cdot x = b$ - system of linear equations (\leftarrow on a rectangular 3-D grid);

 A_{IE} - complex, dense with all entries filled, non-Hermitian matrix; but much more compact than FD and FE matrices

(a) Main attraction: only the scattering volume V^s is subject to discretization;

(this reduce dramatically the size of matrix $A_{\!_{I\!E}}$)

(b) Drawback: most EM software developers refrain from implementation of the IE approach, since accurate computation of the matrix A_{IE} is indeed an extremely tedious and nontrivial problem itself.

$\nabla \times \underline{\mu}^{\mathrm{T}} \mathbf{E} - i\omega \underline{\zeta}(x, y, z, \omega) \mathbf{E} = \mathbf{j}^{ext}$

(2) Finite-difference (FD) approach

 $A_{FD} \cdot x = b$ - system of linear equations (\leftarrow on a rectangular 3D grid);

 A_{FD} - large, sparse 3Mx3M symmetric, non-Hermitian matrix;

 \mathcal{X} represents the grid nodal values of electric field;

b represents the source and boundary conditions

 $M = n_x \cdot n_y \cdot n_z$ - number of model parameters.

(a) The most commonly employed

(b) Main attraction: an apparent simplicity of its numerical implementation

(3) Finite-element (FE) approach

the EM field (or its potentials) are decomposed to some basic (usually, edge and nodal) functions. The coefficients of the decomposition, a vector x_i are sought using the Galerkin method.

$$A_{FE} \cdot x = b$$

 A_{FE} - large, sparse, non-symmetric, non-Hermitian matrix;

- (a) Main attraction: it is commonly believed to be better able than other approaches to accurately account for geometry (shapes of ore-bodies, topography, cylindrical wells, etc.)
- (b) Main drawback: construction of the finite elements themselves is another nontrivial and usually timeconsuming procedure.

• 23d theony · Companison with other approaches •example

x3d statistics: 99x99x11 prisms of 10x10x{10to2000}m³

23 min on a serial PC for 11 frequencies & a single transmitter position;

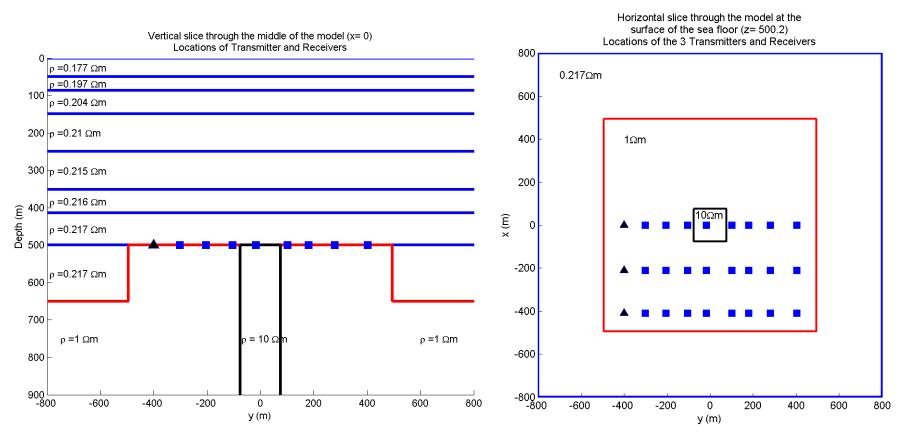


Fig. Marine CSEM model (after Anna Avdeeva)

Time (+) vs Frequency (o): iTr=1, iRcLine=1, NF=5e-025

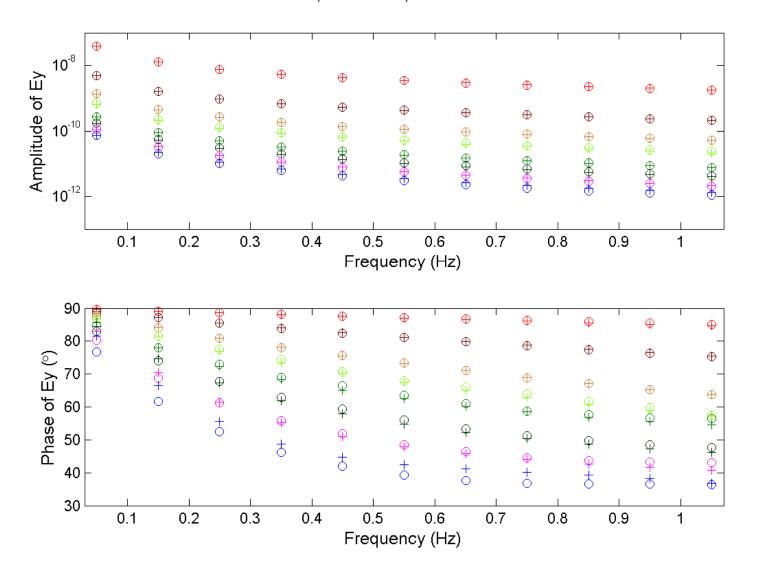
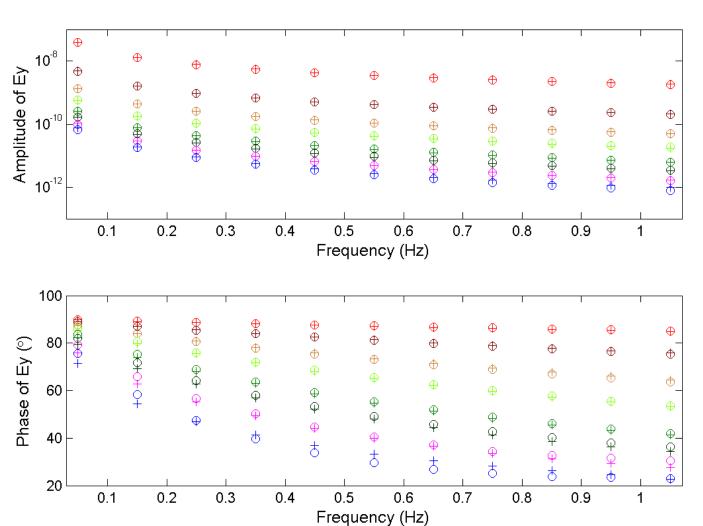


Fig. Comparison x3d code (circles) with another proprietary code (crosses). The amplitudes and phases of Ey component are color-coded for all 8 receiver's positions for profile 1 & 1st transmitter.



Time (+) vs Frequency (o): iTr=3, iRcLine=3, NF=5e-025

Fig. Comparison x3d code (circles) with another proprietary code (crosses). The amplitudes and phases of Ey component are color-coded for all 8 receiver's positions for 3rd profile & 3rd transmitter.

marine csem example

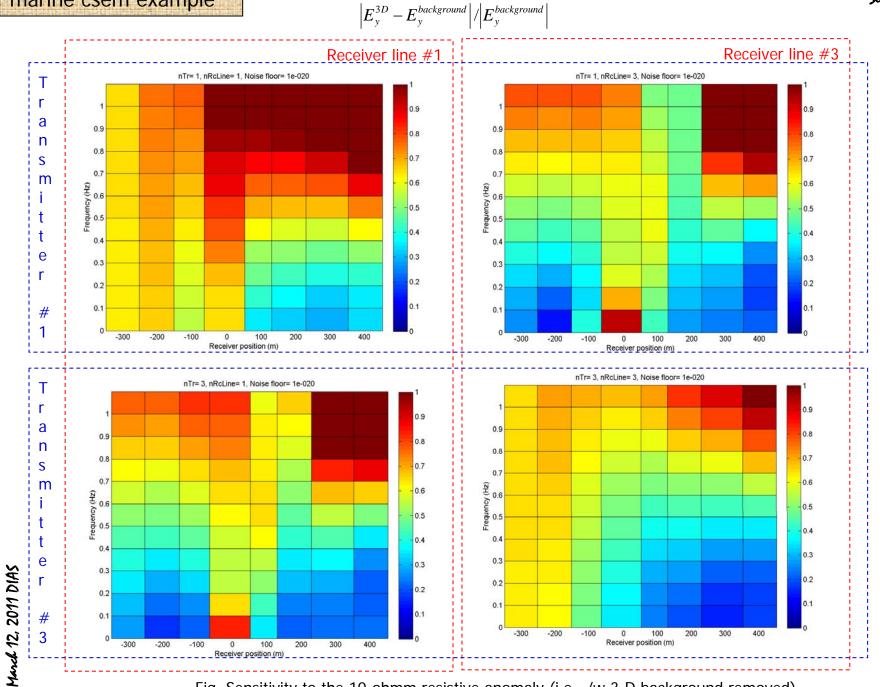


Fig. Sensitivity to the 10-ohmm resistive anomaly (i.e. /w 3-D background removed).

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Thanks to ifm-seomar team (Kiel, Germany) for marine csem simulations

Thank you for your attention