

3D Forward Model

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Goals

- Numerical solution of
 - 3D CSEM induction problems
 - 3D MT problems
- Efficiency increase of numerical scheme by implementation on massively parallel computers



PHYSICAL PROBLEM FORMULATION

Physical problem formulation

- Secondary Coulomb-gauged EM potentials
 - simplify form of Maxwell's equations
 - avoid singularities introduced by sources

Gauged EM potentials

- Magnetic vector potential, \vec{A}
- Electric scalar potential, Φ
- EM potentials are defined by:

$$\vec{B} \equiv \nabla \times \vec{A}$$

$$\vec{E} \equiv i\omega\vec{A} - \nabla\Phi$$

Coulomb gauged formulation

- Simultaneous solution of two equations that constitute incompletely gauged coupled vector-scalar potential formulation of Maxwell's equations:

$$\begin{aligned}\nabla^2 \vec{A} + i\omega\mu_0\sigma(\vec{A} + \nabla\Psi) &= -\mu_0\vec{J}_s \\ \nabla \cdot [i\omega\mu_0\sigma(\vec{A} + \nabla\Psi)] &= 0\end{aligned}$$

- For unique \vec{A} , Coulomb gauge condition must be applied:

$$\nabla \cdot \vec{A} = 0$$

Secondary potential formulation

- Source of arbitrary shape, complexity, and orientation can be introduced by defining set of known primary potentials (\vec{A}_p, Ψ_p)
- Normally, primary potentials are analytic expressions for induction in homogeneous formation of constant electrical conductivity, σ_p

Primary potentials for MT

- EM field of electric dipole at infinity is plane wave
- Natural source is modeled as big electric dipole very far away
- Primary potentials are potentials from dipole source located in homogeneous formation of uniform electrical conductivity, σ_p :

$$\vec{A}_p(\vec{r}) = \frac{I ds}{4\pi r} e^{-kr} \vec{x}$$

Secondary potentials

- (\vec{A}_s, Ψ_s) are defined by:

$$\vec{A} \equiv \vec{A}_p + \vec{A}_s, \quad \Psi \equiv \Psi_p + \Psi_s$$

- Finally, governing equations become:

$$\begin{aligned} \nabla^2 \vec{A}_s + i\omega\mu_0\sigma(\vec{A}_s + \nabla\Psi_s) \\ = -i\omega\mu_0\Delta\sigma(\vec{A}_p + \nabla\Psi_p) \end{aligned}$$

$$\begin{aligned} \nabla \cdot [i\omega\mu_0\sigma(\vec{A}_s + \nabla\Psi_s)] \\ = -\nabla \cdot [i\omega\mu_0\sigma(\vec{A}_p + \nabla\Psi_p)] \end{aligned}$$

Boundary conditions

- Homogeneous Dirichlet boundary condition on outer boundary of domain:

$$(\vec{A}_S, \Psi_S) \equiv (\vec{0}, 0)$$



NUMERICAL SCHEME

Physical problem discretization

- Frequency-domain finite-element (FD-FE) scheme based on unstructured tetrahedral meshes

Solver for resulting system of equations

- Preconditioned complex biconjugate gradient stabilized (BCGStab) algorithm

Parallel implementation

- Domain decomposition technique using
 - master-slave strategy
 - MPI



POSTPROCESS

Postprocess

- Fields $(\vec{E}s, \vec{H}s)$ are obtained from potentials $(\vec{A}s, \Psi s)$ by numerical differentiation:
 - moving least-squares interpolation (MLSI) scheme

MLSI

- Each Cartesian component of \vec{A}_s and Ψ_s are approximated by linear functions:

$$ax + by + cz + d$$

- Spatial derivatives of potentials are first three coefficients (a, b, c)
- MLSI determination of (a, b, c) at arbitrary test point is made in weighted least-squares sense

WLS

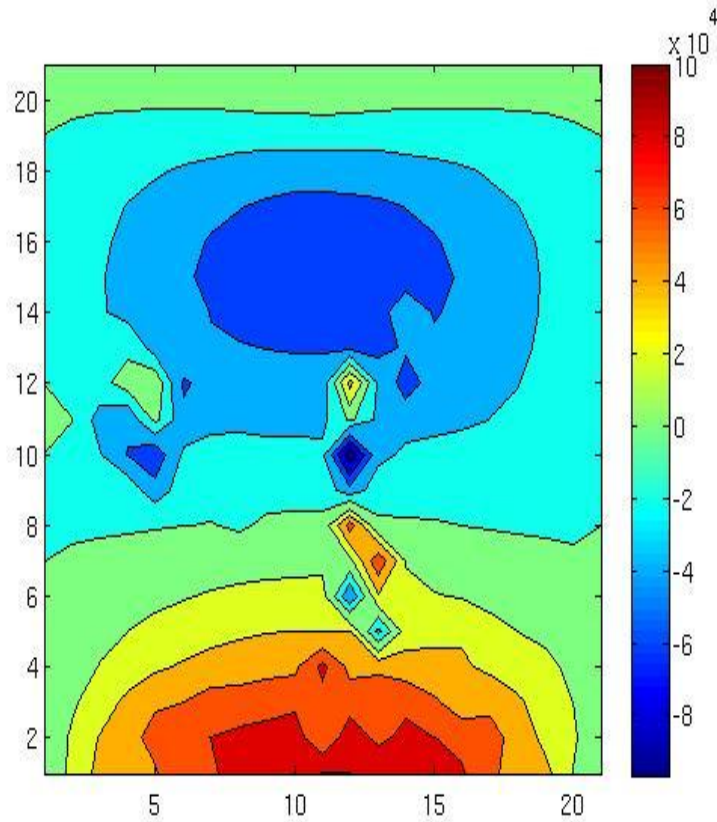
- Minimize sum of weighted squared residuals between linear function and FE-computed values of potentials at $N \sim 30$ nearest nodes to test point
- Weighting function has positive exponential form which is maximum at test point and decreases monotonically with increasing distance away from it

Simple homogeneous half space

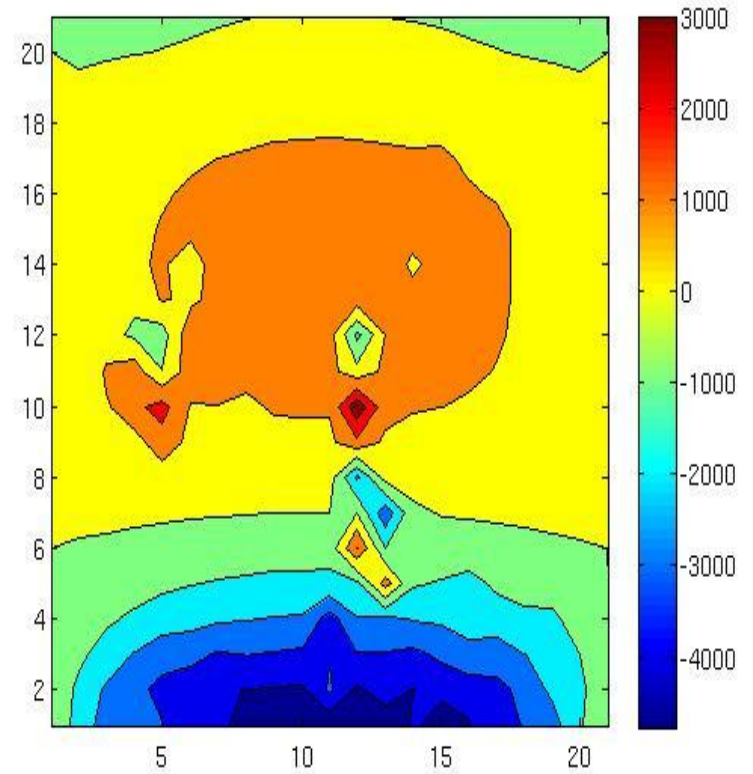


RESULTS

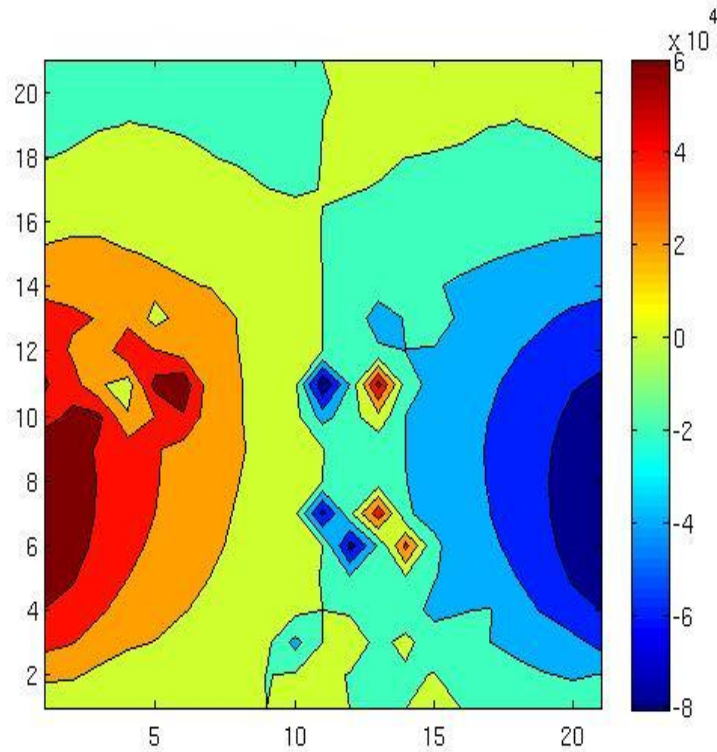
Real part of E_x



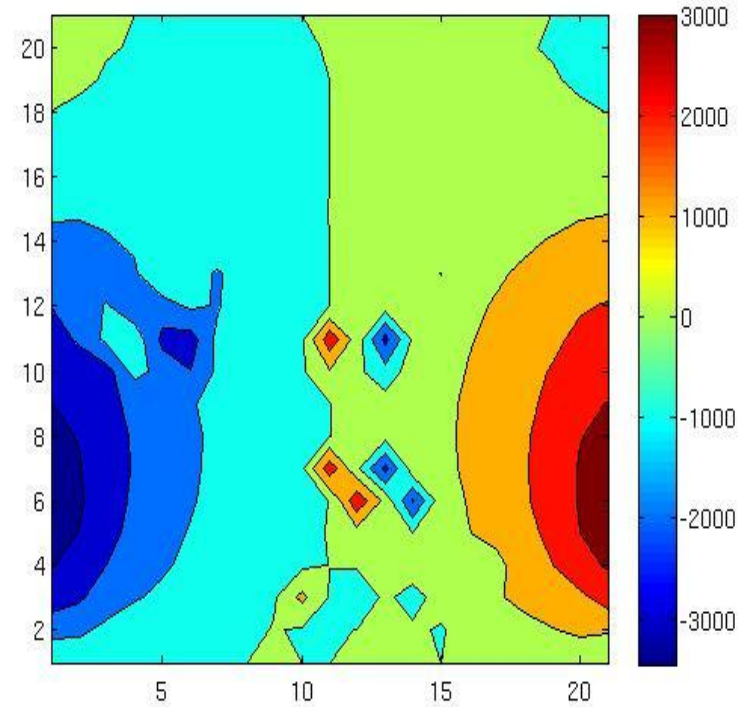
Imaginary part of E_x



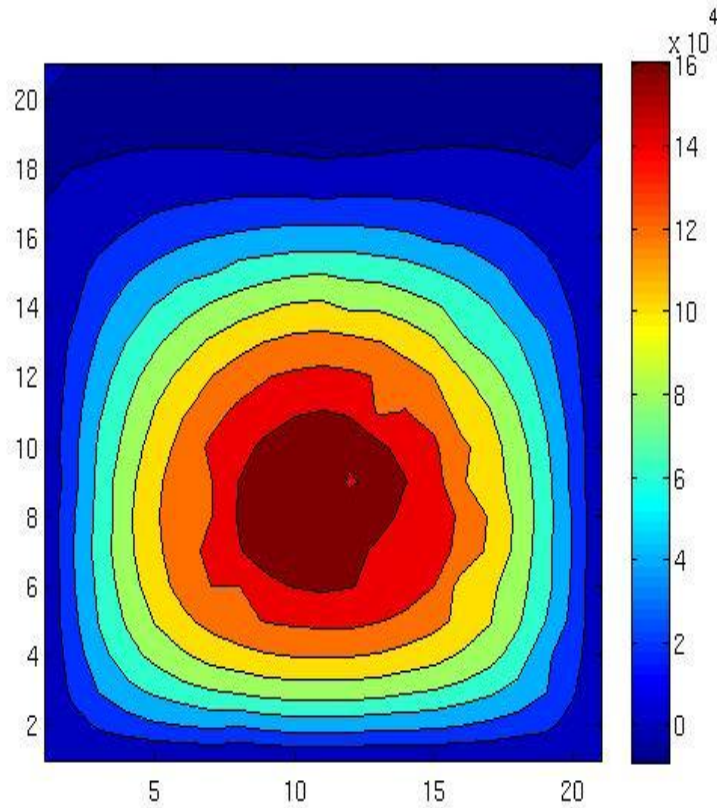
Real part of E_y



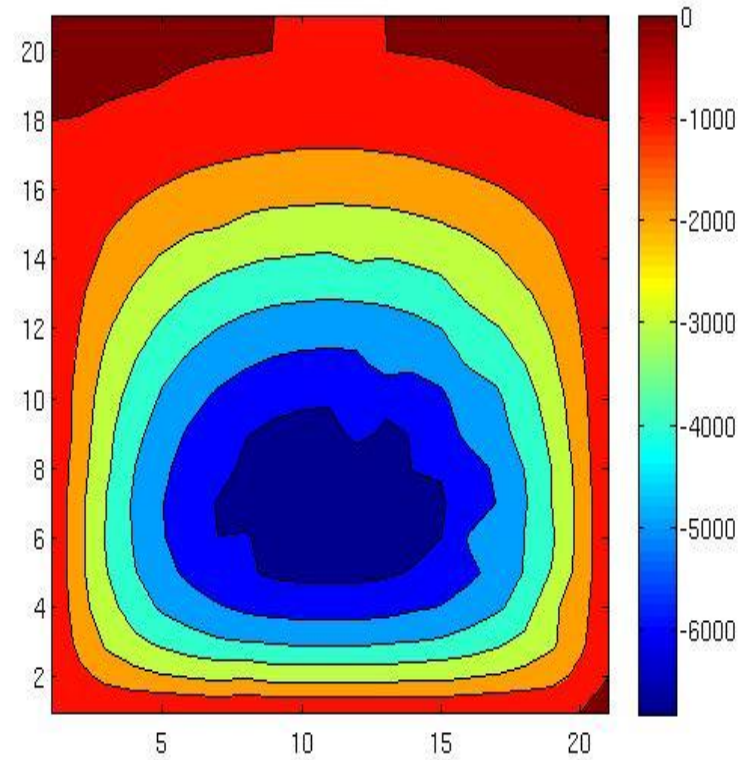
Imaginary part of E_y



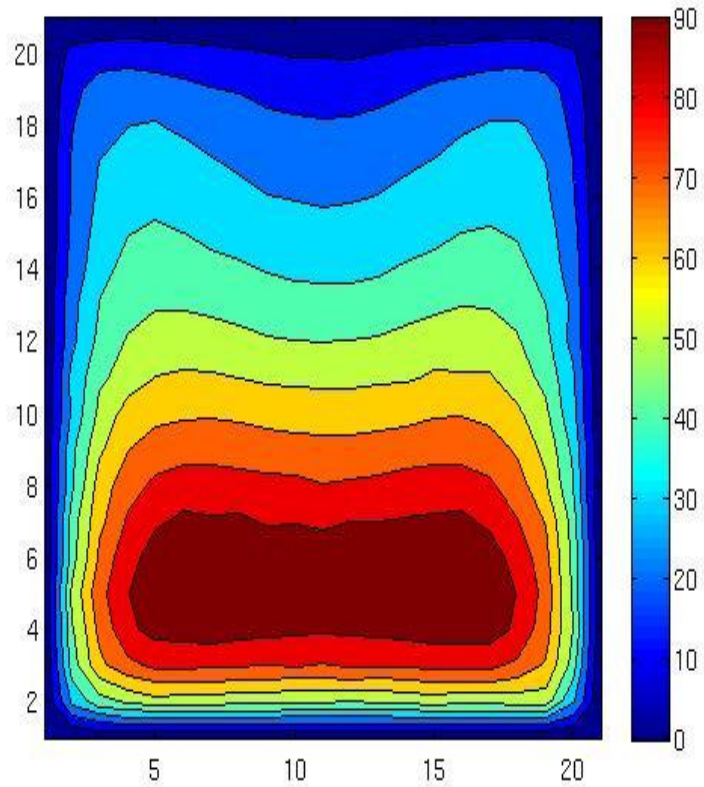
Real part of E_z



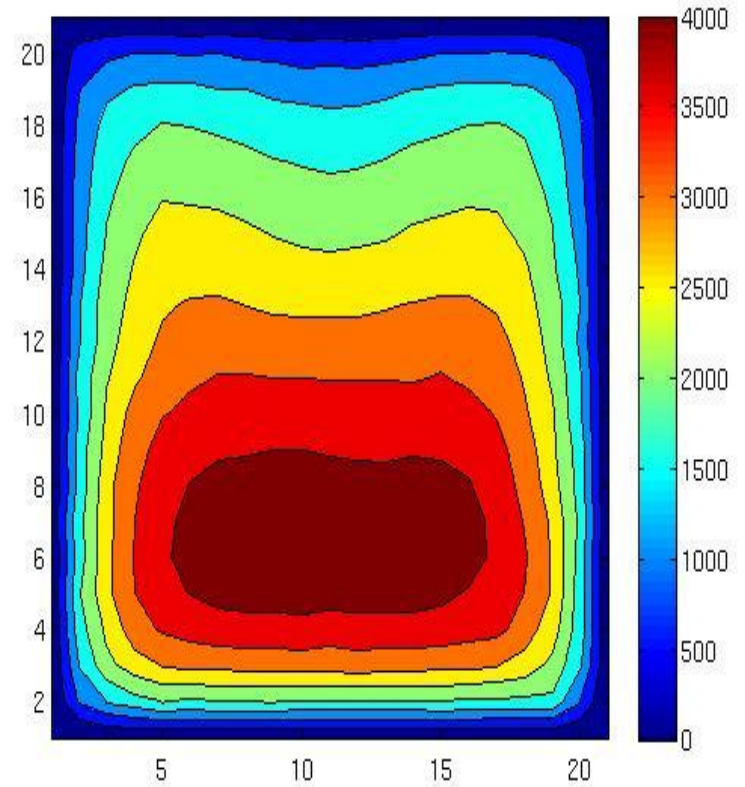
Imaginary part of E_z



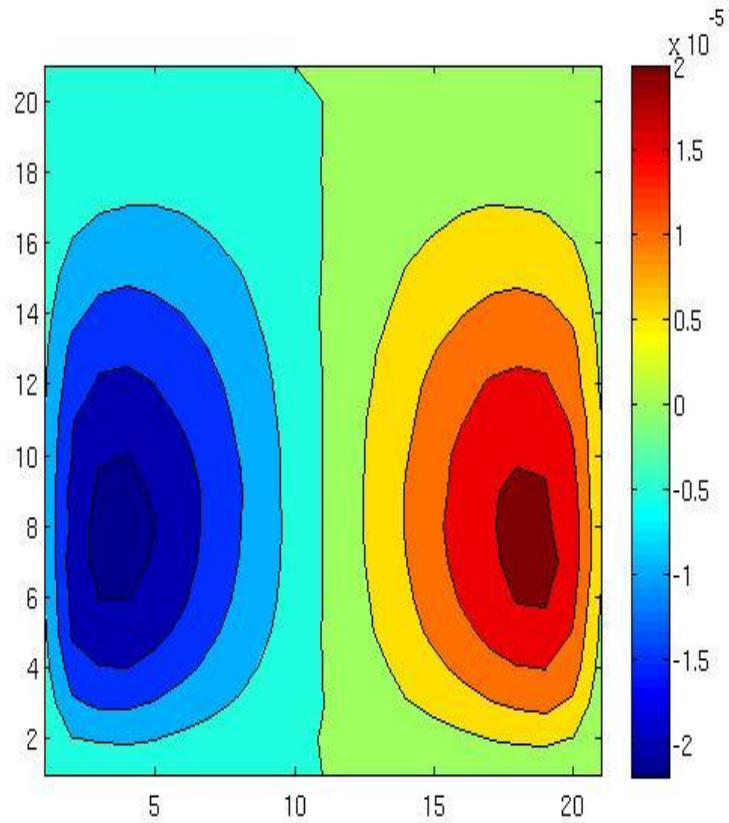
Real part of H_x



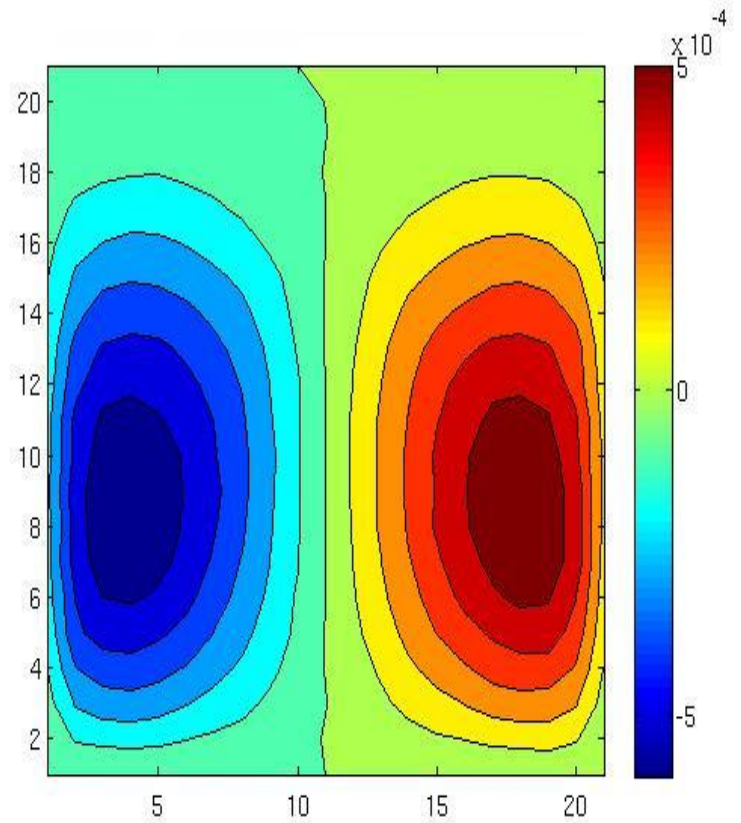
Imaginary part of H_x



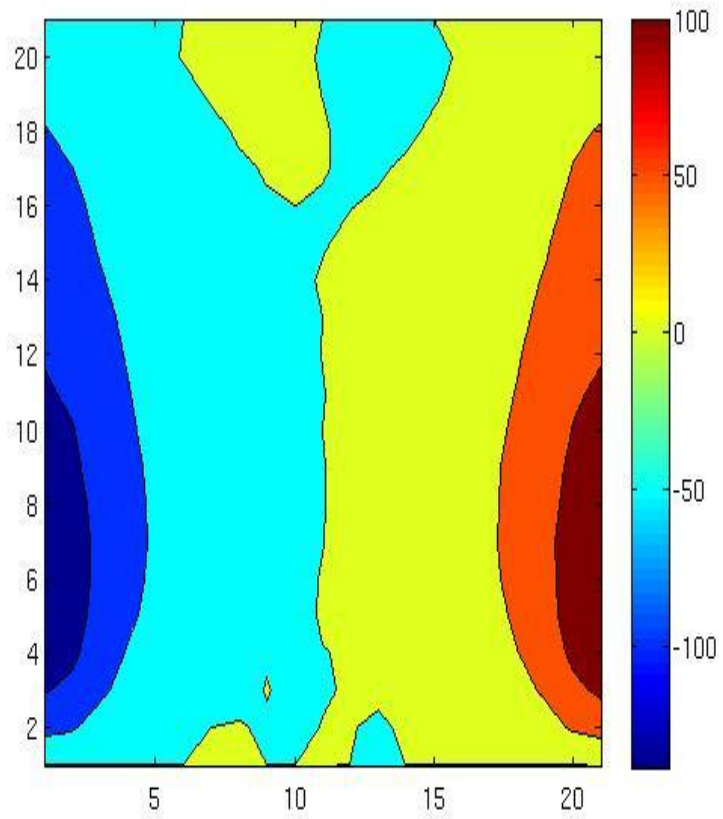
Real part of H_y



Imaginary part of H_y



Real part of Hz



Imaginary part of Hz

