

FINITE-ELEMENT FORWARD SOLVER FOR UNSTRUCTURED TETRAHEDRAL GRIDS

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- 1 Brief explanation of *EM PDE* equations: induction and continuity
- 2 Discretization of the computational domain
- 3 Finite-element method
- 4 Calculating and coding the inner product terms
- 5 Code is under development: Future plans

- Considering a time dependence of $e^{i\omega t}$ in the *Quasi-Static* regime

$$\nabla \times \nabla \times \mathbf{E} + i\omega\mu\tilde{\sigma}\mathbf{E} = i\omega\mu\mathbf{J}^s \quad (1)$$

$$\tilde{\sigma} = \tilde{\sigma}(x, y, z) \text{ and } \mathbf{E} = \mathbf{E}(x, y, z, t)$$

A- ϕ decomposition: To Visualize the *Inductive* and *Galvanic* nature of the EM fields

$$\mathbf{E} = -i\omega\mathbf{A} - \nabla\phi \quad (2)$$

$$\nabla \times \nabla \times \mathbf{A} + i\omega\mu\tilde{\sigma}\mathbf{A} + \mu\tilde{\sigma}\nabla\phi = \mu\mathbf{J}^s \quad (3)$$

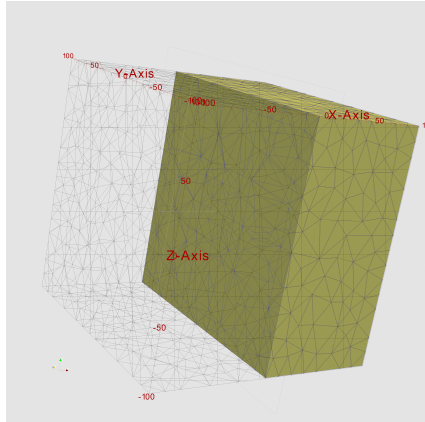
- Setting up the second equation using the Ampère's law

$$\nabla \cdot \mathbf{J} = \begin{cases} -\nabla \cdot \mathbf{J}^s & \text{source location} \\ 0 & \text{otherwise} \end{cases} \quad (4)$$

Because $\mathbf{J} = \tilde{\sigma}\mathbf{E}$,

$$-i\omega\nabla \cdot (\tilde{\sigma}\mathbf{A}) - \nabla \cdot (\tilde{\sigma}\nabla\phi) = -\nabla \cdot \mathbf{J}^s \quad (5)$$

- *Blocks2mesh* a code written by *Peter Lelievre* <plelievre@mun.ca>, is used to create a three dimensional grid of unstructured tetrahedrons
- The code makes a block poly file that get fed into **Tetgen**
- Auxiliary subroutines to set up the connectivity arrays:
 - 1 edge - to - node
 - 2 edge - to - element
 - 3 element - to - edge
 - 4 ...
- Figure is generated by *Kitware Paraview 3.6.2*



THEOREM

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$$\nabla \times \nabla \times \mathbf{A} + i\omega\mu\tilde{\sigma}\mathbf{A} + \mu\tilde{\sigma}\nabla\phi = \mu\mathbf{J}^s$$

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$$-i\omega\nabla \cdot (\tilde{\sigma}\mathbf{A}) - \nabla \cdot (\tilde{\sigma}\nabla\phi) = -\nabla \cdot \mathbf{J}^s$$

is achieved.

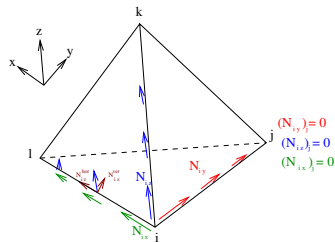
- Finite-element solution
- Approximation of the vector and scalar potentials

$$\tilde{\mathbf{A}} = \sum_{j=1}^{N_{edges}} \tilde{A}_j \mathbf{N}_j \quad (6)$$

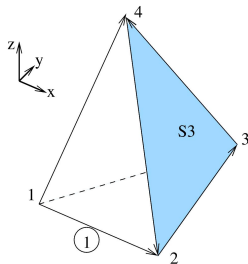
$$\tilde{\phi} = \sum_{k=1}^{N_{nodes}} \tilde{\phi}_{k_1} N_{k_1} \quad (7)$$

- \mathbf{N}_j is the edge-element vector basis function
- and N_{k_1} is the nodal-element scalar basis function

- $N_k^e(x, y, z) = \frac{1}{6V^e} (a_k^e + b_k^e x + c_k^e y + d_k^e z)$
- The scalar basis function N_i is equal to unity at node i and decreases linearly in all three orthogonal directions.
- Vanishes linearly towards the other nodes and faces \rightarrow guarantees the continuity of the tangential \mathbf{E} .
- The vertical component of the \mathbf{E} is not necessarily continuous.



- Edge-elements
- Combines three components into one vector
- tangential components are continuous while verticals are allowed to jump
- Linear Whitney 1-form functions
- $\mathbf{N}_i^e = l_i^e (N_{i1}^e \nabla N_{i2}^e - N_{i2}^e \nabla N_{i1}^e)$



- Seeks the solution by weighting the residual of the differential equation

$$\mathbf{r} = \nabla \times \nabla \times \mathbf{A} + i\omega\mu\tilde{\sigma}\mathbf{A} + \mu\tilde{\sigma}\nabla\phi - \mu\mathbf{J}^s \quad (8)$$

$$R = \int_{\Omega} \mathbf{N}_i \cdot \mathbf{r} \, d\Omega = 0 \quad (9)$$

- Combining (8) and (9) and using the Green's theorem

$$\begin{aligned} \sum_{j=1}^{N_{edges}} \tilde{A}_j \int_{\Omega} (\nabla \times \mathbf{N}_i) \cdot (\nabla \times \mathbf{N}_j) \, d\Omega + i\omega\mu \sum_{j=1}^{N_{edges}} \tilde{A}_j \int_{\Omega} \tilde{\sigma} \mathbf{N}_i \cdot \mathbf{N}_j \, d\Omega \\ + \mu \sum_{k=1}^{N_{nodes}} \phi_k \int_{\Omega} \tilde{\sigma} \mathbf{N}_i \cdot \nabla N_{k_1} \, d\Omega = \mu \sum_{j=1}^{N_{edges}} \int_{\Omega} \mathbf{N}_i \cdot \mathbf{J}_s \, d\Omega \end{aligned} \quad (10)$$

$$k_1 = 1 \cdots N_{nodes}$$

$$i = 1 \cdots N_{edges}$$

$$j = 1 \cdots N_{edges}$$

$$r = i\omega \nabla \cdot (\tilde{\sigma} \mathbf{A}) - \nabla \cdot \tilde{\sigma} \nabla \phi$$

$$R_{scalar} = \int_{\Omega} N_{k_2} r \, d\Omega = 0$$

$$\begin{aligned}
 & i\omega \tilde{A}_j \sum_{j=1}^{N_{edges}} \int_S N_{k_2} \hat{n} \cdot (\tilde{\sigma} \mathbf{N}_j) \, dS - i\omega \tilde{A}_j \sum_{j=1}^{N_{edges}} \int_{\Omega} \nabla N_{k_2} \cdot (\tilde{\sigma} \mathbf{N}_j) \, d\Omega \\
 & + \tilde{\phi}_{k_1} \sum_{k_1=1}^{N_{nodes}} \int_S N_{k_2} \hat{n} \cdot (\tilde{\sigma} \nabla N_{k_1}) \, dS - \tilde{\phi}_{k_1} \sum_{k_1=1}^{N_{nodes}} \int_{\Omega} \nabla N_{k_2} \cdot (\tilde{\sigma} \nabla N_{k_1}) \, d\Omega \quad (11) \\
 & = \int_{\Omega} N_{k_2} \nabla \cdot \mathbf{J}_s \, d\Omega
 \end{aligned}$$

$$k_1 = 1 \cdots N_{nodes}$$

$$k_2 = 1 \cdots N_{nodes}$$

$$j = 1 \cdots N_{edges}$$

- Edge - Edge Products

$$\mathbf{T}_{ij} = \sum_{j=1}^{N_{edges}} \int_{\Omega} (\nabla \times \mathbf{N}_i) \cdot (\nabla \times \mathbf{N}_j) d\Omega$$

$$\mathbf{T}_{ij} = \sum_{j=1}^{N_{edges}} \frac{4 l_i l_j}{(6)^4 (V^e)^3} [(b_{i1} c_{j2} - c_{i1} b_{j2})(b_{j1} c_{j2} - c_{j1} b_{j2}) + (d_{i1} b_{j2} - b_{i1} d_{j2})(d_{j1} b_{j2} - b_{j1} d_{j2}) + (c_{i1} d_{j2} - d_{i1} c_{j2})(c_{j1} d_{j2} - d_{j1} c_{j2})] \quad (12)$$

$$\mathbf{U}_{ij} = \sum_{j=1}^{N_{edges}} \int_{\Omega} \bar{\sigma} \mathbf{N}_i \mathbf{N}_j d\Omega$$

$$\mathbf{U}_{ij} = \frac{l_i l_j}{36(V^e)^2} \bar{\sigma} [F_{i2j2} G_{i1j1} - F_{i2j1} G_{i1j2} - F_{i1j2} G_{i2j1} + F_{i1j1} G_{i2j2}] \quad (13)$$

$$F_{ij} = a_i a_j + b_i b_j + c_i c_j.$$

$$G_{ij} = \int_{\Omega} N_i(x, y, z) N_j(x, y, z) d\Omega$$

- Mapping each tetrahedral element into the **simplex (Normalized) coordinate system**

$$G_{ij} = \int_{\Gamma} N_i(u, v, w) N_j(u, v, w) |\mathbf{J}| du dv dw$$

$$G_{ij} = \begin{cases} \frac{V^e}{10} & i = j \\ \frac{V^e}{20} & i \neq j \end{cases} \quad (14)$$

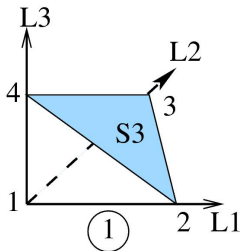
- Connectivity arrays used : Edge - to - edge

- 1 Edge - to - cells
- 2 Cell - to - edges

- Edge - node products

$$\mathbf{w}_{ik} = \int_{\Omega} \bar{\sigma} \mathbf{N}_i \cdot \nabla N_k d\Omega$$

- Mapping into the normalize coordinate system



$$\int_{\Omega} N_i dx dy dz = \int_{\Gamma} N_i(u, v, w) |\mathbf{J}| du dv dw \quad (15)$$

$$\int_{\Omega} N_i dx dy dz = \frac{1}{24} |\mathbf{J}|$$

$$\mathbf{w}_{ik} = \sum_{i=1}^{N_{edges}} \frac{1}{144 V^e} l_i \bar{\sigma} [(b_{i2} b_k + c_{i2} c_k + d_{i2} d_k) - (b_{i1} b_k + c_{i1} c_k + d_{i1} d_k)] \quad (16)$$

- Connectivity arrays used

- 1 Edge - to - cells
- 2 cell - to - nodes

- Node - node products

$$\mathbf{z}_{\mathbf{k}_2 \mathbf{k}_1} = \int_{\Omega} \nabla N_{\mathbf{k}_2} \cdot \bar{\sigma} \nabla N_{\mathbf{k}_1} d\Omega$$

$$\mathbf{z}_{\mathbf{k}_2 \mathbf{k}_1} = \bar{\sigma} \left(\frac{1}{6V^e} \right) [b_{k_2} b_{k_1} + c_{k_2} c_{k_1} + d_{k_2} d_{k_1}] \quad (17)$$

- Connectivity array used: Cell - to - nodes

Source terms

- Edge - Source product

$$\mathbf{S} = \int_{\Omega} \mathbf{N}_i \cdot \mathbf{J}_s d\Omega \quad (18)$$

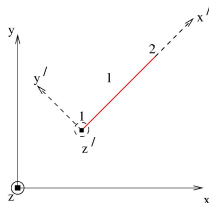
$$\mathbf{S} = \mu \sum_{i=1}^{N_{edges}} \left(\frac{1}{6V^e} \right)^2 (a_{i1} b_{i2} - a_{i2} b_{i1}) j_s l \quad (19)$$

- Node - Source product

$$\mathbf{SS} = \int_{\Omega} N_{\mathbf{k}_2} \nabla \cdot \mathbf{J}_s d\Omega \quad (20)$$

$$\mathbf{SS} = \sum_{k=1}^{N_{nodes}} b_k j_s \left(\frac{1}{6V^e} \right) l \quad (21)$$

- A line source of current is chosen to be a delta function of finite length



$$\mathbf{J} = \delta(y') \delta(z') \text{Box}(x') j_s \hat{\mathbf{x}}' \quad (22)$$

- j_s is an arbitrary scalar quantity; $\text{Box}(x')$ is the boxcar function.

$$\text{Box}(x') = \begin{cases} 0 & x' > l, x' < 0 \\ 1 & 0 < x' < l \end{cases} \quad (23)$$

- **Boundary Conditions**
- BCs are applied to the potentials on the truncation boundaries

$$\hat{n} \times \mathbf{A}|_{\partial\Omega} = \mathbf{0} \quad (24)$$

$$\phi|_{\partial\Omega} = 0 \quad (25)$$

- **System of Equations**
- A large system of equations is constructed

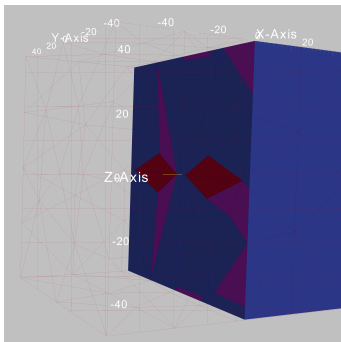
$$\mathbf{L} \cdot \mathbf{u} = \mathbf{F}$$

$$\begin{pmatrix} \mathbf{T}_{ij} & -\omega\mu\mathbf{U}_{ij} & \mu\mathbf{W}_{ik_1} & 0 \\ \omega\mu\mathbf{U}_{ij} & \mathbf{T}_{ij} & 0 & \mu\mathbf{W}_{ik_1} \\ 0 & \omega\mathbf{W}_{k_2j} & -\mathbf{Z}_{k_2k_1} & 0 \\ -\omega\mathbf{W}_{k_2j} & 0 & 0 & -\mathbf{Z}_{k_2k_1} \end{pmatrix} \begin{pmatrix} \mathbf{A}_j^r \\ \mathbf{A}_j^I \\ \phi_k^r \\ \phi_k^I \end{pmatrix} = \begin{pmatrix} \mathbf{S} \\ \mathbf{0} \\ \mathbf{SS} \\ 0 \end{pmatrix} \quad (26)$$

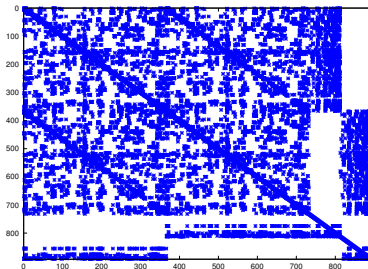
- Dimensions: $\mathbf{L} (2(N_{edges} + N_{nodes}), 2(N_{edges} + N_{nodes}))$
- $\mathbf{u} (2(N_{edges} + N_{nodes}))$
- $\mathbf{S} (2(N_{edges} + N_{nodes}))$

EXAMPLE FOR A COARSE MESH

- $N_{cells} = 216, N_{nodes} = 80, N_{edges} = 366$



- Sparse structure of the coefficient matrix



$$\begin{pmatrix} \mathbf{T}_{ij} & -\omega\mu\mathbf{U}_{ij} & \mu\mathbf{W}_{ik_1} & 0 \\ \omega\mu\mathbf{U}_{ij} & \mathbf{T}_{ij} & 0 & \mu\mathbf{W}_{ik_1} \\ 0 & \omega\mathbf{W}_{k_2j} & -\mathbf{Z}_{k_2k_1} & 0 \\ -\omega\mathbf{W}_{k_2j} & 0 & 0 & -\mathbf{Z}_{k_2k_1} \end{pmatrix}$$

- The code is under development. We hope to apply it to simple Earth models
- The non-symmetric system of equations will be solved using **BICGSTAB** solver with an **LU** preconditioner
- The performance of the above approach will be compared with a modification in which the **Lorentz gauge condition** is used. Also, the relative contributions to the electric field from the **inductive and galvanic** terms will be investigated in different situations.